

HYBRID OF PREDICTIVE AND CLOSED-LOOP PHASE-DOMAIN DIGITAL PLL ARCHITECTURE

Related Patent Applications

5 This application claims the benefit, under 35 U.S.C. §119(e)(1), of U.S. Provisional Application No. 60/186,251, entitled *Hybrid of predictive/closed-loop digital PLL operation*, filed March 1, 2000 by Robert B. Staszewski and Dirk Leipold; and U.S. Provisional Application No. 60/198,907, entitled *PLL loop compensation scheme for the frequency/phase modulation*, filed April 20, 2000 by Robert B. Staszewski, Ken Maggio and Dirk Leipold.

10 This application is related to U.S. Patent Application S/N 09/603,023, entitled *Digital Phase-Domain PLL Frequency Synthesizer*, docket number TI-30677, filed June 26, 2000, by Robert B. Staszewski and Dirk Leipold; and U.S. Patent Application S/N 09/608,317, entitled *Digital Fractional Phase Detector*, docket number TI-30676, filed 15 June 30, 2000, by Robert B. Staszewski and Dirk Leipold, both applications assigned to the assignee of the present invention and incorporated by reference in their entirety herein.

20 **Background of the Invention**

1. Field of the Invention

This invention relates generally to phase lock loops, and more particularly to an all-digital phase-domain phase-lock loop (PLL) that employs a hybrid of predictive and closed-loop architectures.

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2. Description of the Prior Art

Open-loop modulation techniques for data transmission are well-known in the prior art, and exhibit undesirable frequency wander and drift. Feed forward, closed-loop compensation techniques with phase-locked loop compensation for data transmission and phase

is only approximate because of component matching difficulties and disagreement between the transfer functions.

The idea of phase compensating a phase locked loop (PLL) by digitally integrating the transmit modulating data bits and using the integrator output to shift the 5 phase of the reference clock signal, while the Gaussian filtered data directly frequency modulates the VCO has been disclosed by M. Bopp et al., "A DECT transceiver chip set using SiGe technology," *Proc. of IEEE Solid-State Circuits Conf.*, sec. MP4.2, pp. 68-69, 447, Feb. 1999. This approach however, is rather analog in nature and therefore requires precise component matching, of not only the VCO, but also the phase shifter.

10 A similar feed-forward compensation method which also requires a precise knowledge of the ever-changing model of the VCO and other analog circuits has been disclosed by B. Zhang, P. Allen, "Feed-forward compensated high switching speed digital phase-locked loop frequency synthesizer," *Proc. Of IEEE Symposium on Circuits and Systems*, vol.4, pp. 371-374, 1999.

15 In view of the foregoing, it is highly desirable to have a digitally-intensive PLL architecture that is compatible with modern CMOS technology in order to reduce parameter variability generally associated with analog circuits.

Summary of the Invention

The present invention is directed to a hybrid of a predictive and closed-loop PLL technique and its most preferred application to implement a direct oscillator transmit modulation. An all-digital type-I PLL loop includes a digitally-controlled oscillator (DCO) where the DCO control and resulting phase error measurements are in numerical format. The current gain of the DCO is easily predicted by simply observing the past phase error responses to the DCO. With a good estimate of the current oscillator gain, normal DCO control can then be augmented with the “open loop” instantaneous frequency jump estimate of the new frequency control word command. The resulting phase error is expected to be very small and subject to the normal closed PLL loop correction transients.

According to one embodiment, a digital phase-locked loop with a modulation circuit comprises:

a digital phase-locked loop having a phase detector, a loop filter and a digitally-controlled oscillator (DCO), wherein the DCO is responsive to an oscillator tuning word (OTW) to generate a DCO output clock, and further wherein the phase detector is responsive to a channel selection signal, a modulating data signal and the output clock generated by the DCO to generate a phase detector output signal, and further wherein the loop filter generates a filtered phase error in response to the output signal generated by the phase detector; and

a direct modulator operational in response to the filtered phase error and the modulating signal to generate the OTW.

According to another embodiment, a phase-locked loop with a modulation circuit comprises:

a digitally-controlled oscillator responsive to an oscillator tuning word (OTW) to generate an oscillator output clock;

a direct modulator operational in response to a modulating signal and a filtered

an accumulator circuit operational in response to a frequency division ratio command, the modulating data signal and clock edge counts associated with the oscillator output clock to generate the phase error.

According to still another embodiment of the present invention, a digital phase-
5 domain phase-locked loop circuit comprises:

- a digitally-controlled oscillator (DCO);
- a gain element feeding the DCO and operational to compensate DCO gain in response to a loop gain signal such that the DCO gain will have substantially no effect on loop behavior;
- 10 an oscillator phase accumulator operational to accumulate DCO generated clock edges;
- a reference phase accumulator operational to accumulate a frequency division ratio command and a modulating data signal and to generate an accumulated frequency control word (FCW) therefrom;
- 15 a phase detector operational to compare the accumulated FCW and the accumulated DCO generated clock edges and generate a phase error in response thereto; and
- a direct modulator operational in response to the modulating data signal and the phase error to generate the loop gain signal.

According to still another embodiment of the present invention, a method of operating a phase-locked loop having a digitally-controlled oscillator comprises the steps of:

- (a) providing a phase-locked loop including a digitally-controlled oscillator (DCO) having a gain K_{DCO} , a phase detector, and a loop filter, wherein the DCO is responsive to an oscillator tuning word (OTW) to generate a DCO output clock having a frequency f_{OTW} , and further wherein the phase detector is responsive to a channel selection signal, a modulating data signal and the output clock to generate a phase detector output signal, and further wherein the loop filter generates a filtered phase error in response to

- (b) providing a direct modulator operational in response to the filtered phase error and the modulating data signal to generate the OTW;

(c) communicating a channel selection signal to the phase detector and simultaneously communicating a calibration modulating data signal to both the phase detector and the direct modulator, and observing a change $\Delta\phi$ in the phase detector output signal in response to a given change Δx in the OTW; and

5 (d) estimating a DCO gain \hat{K}_{DCO} , defined by $\hat{K}_{DCO} = \frac{\Delta\phi}{\Delta x} \cdot f_{ref}$ such that the DCO

gain K_{DCO} can be compensated to substantially remove its effects on loop behavior.

In one aspect of the invention, a hybrid of predictive and closed PLL loop techniques is used to estimate and compensate for the gain of a DCO.

10 In another aspect of the invention, a hybrid of predictive and closed PLL loop techniques is used to minimize undesirable parameter variability normally associated with analog circuits.

In yet another aspect of the invention, a hybrid of predictive and closed PLL loop techniques is used to directly implement oscillator frequency/phase transmit modulation to minimize system transmitter requirements.

15 In still another aspect of the invention, a hybrid of predictive and closed PLL loop techniques is used to implement an all-digital phase-domain PLL frequency synthesizer that accommodates the “BLUETOOTH” standard.

20 In still another aspect of the invention, a hybrid of predictive and closed PLL loop techniques employs fractional phase error correction such that a digitally-controlled oscillator gain can be compensated to substantially remove its effects on PLL loop behavior.

Brief Description of the Drawings

Other aspects and features of the present invention and many of the attendant advantages of the present invention will be readily appreciated as the same become better understood by reference to the following detailed description when considered in connection with the accompanying drawings in which like reference numerals designate like parts throughout the figures thereof and wherein:

5 Figure 1 is a simplified block diagram illustrating a phase-domain all-digital synchronous PLL loop synthesizer;

10 Figure 2 is a simplified block diagram that exemplifies fractional phase error correction implemented with the phase-domain all-digital synchronous PLL loop synthesizer depicted in Figure 1;

15 Figure 3 is a block diagram illustrating direct oscillator modulation with a straightforward PLL loop compensation scheme according to one embodiment of the present invention;

Figure 4 is a block diagram illustrating direct oscillator modulation with a PLL loop compensation scheme according to another embodiment of the present invention;

20 Figure 5 is a block diagram illustrating partially-direct oscillator modulation with a PLL loop compensation scheme according to one embodiment of the present invention;

25 Figure 6 is a block diagram illustrating partially-direct oscillator modulation with a PLL loop compensation scheme according to another embodiment of the present invention;

Figure 7 is a block diagram illustrating direct oscillator modulation with a PLL loop compensation within a general digital PLL architecture according to one embodiment of the present invention; and

Figures 8(a)-8(d) show a simulated response of the closed-loop type-I *all-digital phase-locked loop* (ADPLL) synthesizer illustrated in Figure 5 to the direct BT=0.5 GFSK modulation ("BLUETOOTH" specification) with the loop compensation

While the above-identified drawing figures set forth alternative embodiments, other embodiments of the present invention are also contemplated, as noted in the

discussion. In all cases, this disclosure presents illustrated embodiments of the present invention by way of representation and not limitation. Numerous other modifications and embodiments can be devised by those skilled in the art which fall within the scope and spirit of the principles of this invention.

Detailed Description of the Preferred Embodiments

Figure 1 is a simplified block diagram illustrating a phase-domain all-digital synchronous PLL loop synthesizer 100. Synthesizer 100 is described more fully in U.S. Patent Application S/N 09/603,023 referenced above and is incorporated by reference herein in its entirety. At the heart of the synthesizer 100 lies a digitally-controlled oscillator (DCO) 102 with a physically-inherent gain of K_{DCO} , defined as an oscillating frequency deviation from the carrier (in Hz) in response to 1 LSB of the input change. DCO 102 is described more fully in U.S. Patent Application entitled *Digitally-Controlled L-C Oscillator*, docket number TI-30695, filed on October 5, 2000 by Robert B. Staszewski and Dirk Leipold which is incorporated by reference herein in its entirety. The DCO 102 oscillator, together with the DCO gain normalization f_{ref} / \hat{K}_{DCO} multiplier 104, logically comprise the normalized DCO (nDCO) 106. The DCO 102 gain normalization decouples the phase and frequency information throughout the system 100 from the process, voltage and temperature variations. The phase information is normalized to 2π radians of the oscillator 102, whereas the frequency information is normalized to an external reference frequency f_{ref} . As described herein below, the \hat{K}_{DCO} estimate is another input and is calculated entirely in the digital domain by observing the past phase error responses to the previous DCO 102 or nDCO 106 phase error corrections.

A normalized loop gain α multiplier 108 can be seen feeding the nDCO 106. The normalized proportional loop gain constant α is a programmable PLL loop parameter that controls the loop bandwidth. It is defined as how much phase attenuation is expected to be observed at the phase detector output in response to a certain change in the phase detector output at the previous reference clock cycle.

The PLL loop is a synchronous all-digital phase-domain architecture that arithmetically compares the accumulated *frequency control word* (FCW) in the reference phase accumulator $R_{ref}(k)$ 110 with the DCO 102 clock edge count in the variable phase

30 coarse integer phase error being compensated by the finer fractional error correction in

order to increase the phase resolution of the system 100, such as described in U.S. Patent Application S/N 09/608,317 referenced herein above. The FCW input 114 to the reference phase accumulator 110 is used to establish the operating frequency of the desired channel and it is expressed in a fixed-point format such that 1 LSB of its integer 5 part corresponds to the f_{ref} reference frequency. Figure 2 is a simplified block diagram that exemplifies fractional phase error correction 200 implemented with the phase-domain all-digital synchronous PLL loop synthesizer 100 depicted in Figure 1.

With continued reference now to Figure 1, the oscillating frequency f_r 116 could be dynamically controlled by directly adding the modulating data $y(k)$ to the channel 10 command of the reference phase accumulator input FCW 114. Generally, direct frequency or phase transmit modulation of a PLL loop of a RF frequency synthesizer is rather a challenging task. In order to attenuate the reference spurs, the PLL bandwidth is usually kept low. This effectively prevents an application of closed loop modulation if the modulating data rate is not much smaller than the loop bandwidth. The direct closed-loop 15 modulation of the DCO frequency 116 is considered however, to be a more cost effective solution than the alternative of an image reject quadrature modulator.

Taking advantage of the predictive capabilities of the all-digital PLL loop as now described below could dramatically enhance the PLL loop operation. The nDCO 106 does not necessarily have to follow the modulating FCW command discussed herein 20 above with the normal PLL loop response. In the phase-domain all-digital synchronous PLL loop synthesizer 100 shown in Figures 1 and 2, for example, where the nDCO 106 control and the resulting phase error measurement are in numerical format, it is easy to predict the current \hat{K}_{DCO} gain of the oscillator 106 by simply observing the past phase error responses to the previous DCO 102 or nDCO 106 corrections. With a good 25 estimate of the \hat{K}_{DCO} gain, the normal DCO control could be augmented with the "open loop" instantaneous frequency jump estimate of the new FCW command. The resulting phase error should be small and subject to the normal closed PLL loop correction transients.

the prediction feature is less important for channel hopping, where the allowed time is much greater. It is, however, essential to realize the direct frequency synthesizer

modulation in the *Gaussian frequency shift keying* (GFSK) modulation scheme of “BLUETOOTH” or GSM, as well as the chip phase modulation of the 802.11b or Wideband CDMA.

Figure 3 is a block diagram illustrating a technique 300 for implementing direct oscillator modulation with a straightforward PLL loop compensation scheme according to one embodiment of the present invention. The DCO frequency 116 is directly modulated in a feed-forward manner such that it effectively removes the loop dynamics from the modulating transmit path. The rest of the loop however, including all error sources, operates under the normal closed-loop regime. The modulating data $y(k)$ at the upper feed 302 directly affects the oscillating frequency with the transfer function:

$$h^f_{dir}(k) = \frac{1}{\alpha} \cdot \alpha \cdot \frac{f_R}{\hat{K}_{DCO}} \cdot K_{DCO} = f_R \cdot \frac{K_{DCO}}{\hat{K}_{DCO}} \quad (1)$$

Unfortunately, the PLL loop will try to correct this perceived frequency perturbation integrated over the update period $1/f_R$ and the phase transfer function is:

$$h_{dir}(k) = \frac{1}{f_R} \cdot f_R \cdot \frac{K_{DCO}}{\hat{K}_{DCO}} = \frac{K_{DCO}}{\hat{K}_{DCO}} \quad (2)$$

If the nDCO 106 gain estimate \hat{K}_{DCO} is accurate, the $h_{dir} = 1$.

20 The transfer characteristic of the PLL loop with only the upper feed 302 is high-pass. The low frequency components of the $y(k)$ data will be integrated in the variable accumulator, thus affecting the oscillator frequency base-line. It is necessary, therefore, to add a phase compensating circuit $R_Y(k)$ 304, as shown at the lower $y(k)$ feed 306, that would completely subtract the phase contribution of the upper $y(k)$ direct modulation feed 302 into the PLL loop if the DCO gain could be estimated correctly. The phase compensating transfer function is:

Figure 4 is a block diagram illustrating a technique for implementing direct oscillator modulation with a PLL loop compensation scheme 400 according to another embodiment of the present invention. The PLL loop compensation scheme 400 merges the phase compensation accumulator $R_Y(k)$ 304 with the reference phase accumulator 5 $R_R(k)$ 110. The frequency control word (FCW) now becomes the sum of the channel and modulating data $y(k)$ signals which is more intuitive. This direct oscillator modulation with the PLL compensating scheme 400 works best in a digital implementation since almost perfect compensation can be achieved. It can be appreciated by those skilled in the art that the foregoing scheme 400 will function equally 10 well with a higher order PLL loop.

Figure 5 is a block diagram illustrating a technique for implementing partially- 15 direct oscillator modulation with a PLL loop compensation scheme 500 according to one embodiment of the present invention. When the direct modulation slider 502 gain is set to zero, the transmit modulating data $y(k)$ undergoes the normal attenuation of the PLL loop low-pass filtering characteristics. When the direct modulation slider 502 gain is set to one however, the direct path, left $y(k)$ 504, will fully undo the loop response due to the feedforward transmit data path, right $y(k)$ 506. It can be appreciated the slider 502 gain value could also be set somewhere between the two extremes of 0 and 1 for partial direct modulation. Selective attenuation, as used herein, then means, either no attenuation, 20 complete attenuation, or anything in between the two extremes of no attenuation and complete attenuation.

Figure 6 is a block diagram illustrating a technique for implementing partially- 25 direct oscillator modulation with a PLL loop compensation scheme 600 according to another embodiment of the present invention. If the loop parameter α is simply a power of two, which might seem quite adequate, then the architecture 500 depicted in Figure 5 is a good choice since the *alpha* loop gain multiplier 108, if implemented as a bit shift operator, can be merged with the DCO gain normalization element 602. Those skilled in the art will appreciate implementation of a $1/\alpha$ operator is equally trivial. If, however, a

structure 600 illustrated in Figure 6 is preferred since the inverse operation $1/\alpha$ is no longer necessary.

Figure 7 is a block diagram illustrating direct oscillator modulation with a PLL loop compensation within a general digital PLL architecture 700 according to one embodiment of the present invention. PLL 702 includes a DCO 102, phase detector 704 and loop filter 706. A conventional PLL that could be used to practice the present invention may include a VCO, a frequency prescaler and divider, phase detector, loop filter and a digital to analog converter (DAC) that makes it possible to control the oscillating frequency through a digital word. The modulating data $y(k)$ 710 is dynamically added to the channel frequency information 712 in order to affect frequency or phase of the oscillator 102 output f_V 116. This could be accomplished, for example, by controlling the frequency division ratio of the fractional-N PLL loop 702. The direct modulation structure 720 is inserted somewhere between the loop filter 706 and the oscillator 102 such as depicted in Figure 7. Gain of the direct modulating path from $y(k)$ 710 to the oscillator 102 input should be $\frac{f_{ref}}{K_{DCO}}$ if $y(k)$ is expressed as the unitless fractional division ratio.

The only unknown parameter of the system 700 is the DCO 102 gain K_{DCO} , as discussed herein before. An estimate of the DCO 102 gain K_{DCO} , could be performed entirely in the digital domain by observing the past phase error responses to the previous DCO 102 or nDCO 106 phase error corrections.

$$20 \quad K_{DCO} = \frac{\Delta f}{\Delta x} \quad (4)$$

where, Δf is an oscillating frequency deviation in response to a Δx change to the digital *oscillator tuning word* (OTW) input 730. K_{DCO} should be fairly linear with respect to the input, otherwise, the DCO gain could be generalized as being a function $K_{DCO}(x)$ of the input x (which is OTW).

The frequency deviation Δf can not be readily measured. It can however, be ascertained by observing the accumulated phase $\Delta\phi$ (expressed as a fraction of the DCO 102 clock period) in the observation interval of the phase detector 706 update, which is equal to the frequency reference clock period T_{ref} .

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$$\Delta f = \frac{\Delta\phi}{T_{ref}} = \Delta\phi \cdot f_{ref} \quad (6)$$

Equation 6 can then be combined with equation 5 to provide an estimated gain

$$10 \quad \hat{K}_{DCO}(x) = \frac{\Delta\phi}{\Delta x} \cdot f_{ref} \quad (7)$$

where, equation 7 allows one to calculate the local value, i.e., for a given DCO 102 input x , (which is OTW), of the oscillator gain K_{DCO} by observing the phase detector 704 output $\Delta\phi$ being a response to the Δx input perturbation at the previous reference clock cycle. Naturally, f_{ref} is the system 700 parameter that is, for all practical purposes, known exactly. Those skilled in the art can appreciate that since the phase detector 704 can have a nonzero resolution, a larger Δx may be required to observe a statistically significant response in $\Delta\phi$. Most preferably, the estimate of K_{DCO} is averaged over a number of measurements. The estimate of K_{DCO} can be stored in a table for some period of time. 15 Preferably, the oscillator gain K_{DCO} is re-estimated periodically, especially in response to changes in PLL operating conditions such as temperature and/or voltage changes.

20 Figures 8(a)-8(d) show a simulated response of the closed-loop type-I *all-digital phase-locked loop* (ADPLL) synthesizer 500 illustrated in Figure 5 to the direct BT=0.5 GFSK modulation ("BLUETOOTH" specification) with the loop compensation mechanism 502 depicted in Figure 5 turned on and off. The simulated response was obtained for a normalized loop gain $\alpha = 0.05$, where a critically-damped loop corresponds

25 to a loop bandwidth of 1000 Hz. The loop bandwidth is 1000 Hz, which corresponds to the modulation index of 0.3. The upper Figures 8(a) and 8(c) depict the digital phase detector output to the nDCO 106; and the lower Figures 8(b)

and 8(d) depict the respective instantaneous DCO 102 period deviation in ps units. The fractional phase detector resolution Δt_{res} is 10 ps in each case (transmit modulation loop compensation scheme turned-off in Figures 8(a) and 8(b) and turned-on in Figures 8(c) and 8(d)). A 10 ps resolution can be achieved, for example, using an advanced CMOS process.

5 In summary explanation of the foregoing, reducing the normalized loop gain α to obtain adequately fine frequency resolution decreases the closed-loop PLL bandwidth such that it starts affecting the shape of the modulating 1 Mbps GFSK waveform. A closed-loop modulation method might therefore be adequate for a GSM system where the 10 modulating frequency is on the order of tens of kHz. For "BLUETOOTH" however, and especially for lower normalized loop gain α , it is necessary to amend the straightforward closed-loop GFSK modulation method with a PLL loop compensation scheme that will remove the loop dynamics from the modulating path. The present hybrid of predictive and closed-loop PLL operation achieves the requisite functionality by ensuring that only 15 the modulating path operates in an open-loop fashion, while the rest of the loop, including all error sources, operate under the normal closed-loop regime.

In view of the above, it can be seen the present invention presents a significant advancement in the art of digital PLL schemes and associated methods. This invention has been described in considerable detail in order to provide those skilled in the digital 20 PLL art with the information need to apply the novel principles and to construct and use such specialized components as are required. In view of the foregoing descriptions, it should be apparent that the present invention represents a significant departure from the prior art in construction and operation. However, while particular embodiments of the present invention have been described herein in detail, it is to be understood that various 25 alterations, modifications and substitutions can be made therein without departing in any way from the spirit and scope of the present invention, as defined in the claims which follow. For example, while certain embodiments set forth herein illustrate various hardware implementations, the present invention shall be understood to also parallel